

## GATE SOLVED PAPER - EE

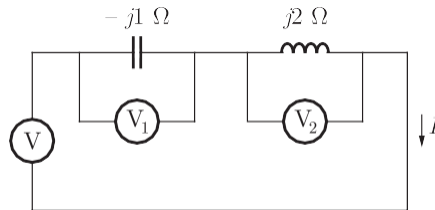
## ELECTRICAL &amp; ELECTRONIC MEASUREMENTS

YEAR 2013

ONE MARK

Q. 1

Three moving iron type voltmeters are connected as shown below. Voltmeter readings are  $V$ ,  $V_1$  and  $V_2$  as indicated. The correct relation among the voltmeter readings is



(A)  $V = \frac{V_1 + V_2}{\sqrt{2}}$

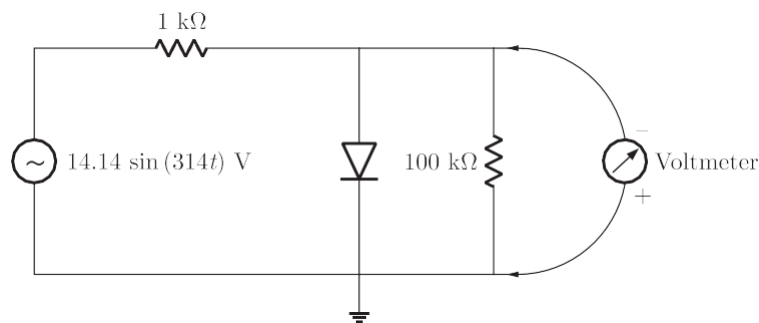
(B)  $V = V_1 + V_2$

(C)  $V = V_1 V_2$

(D)  $V = V_2 - V_1$

Q. 2

The input impedance of the permanent magnet moving coil (PMMC) voltmeter is infinite. Assuming that the diode shown in the figure below is ideal, the reading of the voltmeter in Volts is



(A) 4.46

(B) 3.15

(C) 2.23

(D) 0

YEAR 2013

TWO MARKS

Q. 3

Two magnetically uncoupled inductive coils have  $Q$  factors  $q_1$  and  $q_2$  at the chosen operating frequency. Their respective resistances are  $R_1$  and  $R_2$ . When connected in series, their effective  $Q$  factor at the same operating frequency is

(A)  $q_1 + q_2$

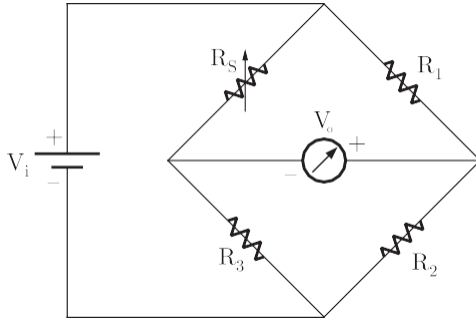
(B)  $\frac{1}{q_1} + \frac{1}{q_2}$

(C)  $\frac{q_1 R_1 + q_2 R_2}{R_1 + R_2}$

(D)  $\frac{q_1 R_2 + q_2 R_1}{R_1 + R_2}$

Q. 4

A strain gauge forms one arm of the bridge shown in the figure below and has a nominal resistance without any load as  $R_s = 300 \Omega$ . Other bridge resistances are  $R_1 = R_2 = R_3 = 300 \Omega$ . The maximum permissible current through the strain gauge is 20 mA. During certain measurement when the bridge is excited by maximum permissible voltage and the strain gauge resistance is increased by 1% over the nominal value, the output voltage  $V_0$  in mV is



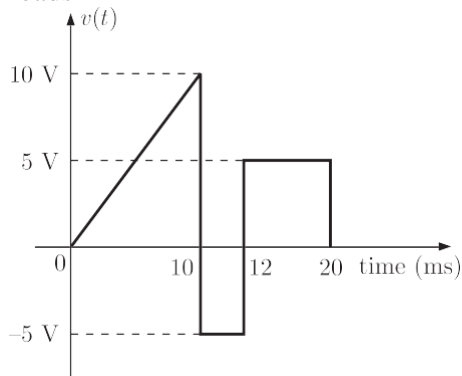
- (A) 56.02
- (B) 40.83
- (C) 29.85
- (D) 10.02

YEAR 2012

ONE MARK

Q. 5

A periodic voltage waveform observed on an oscilloscope across a load is shown. A permanent magnet moving coil (PMMC) meter connected across the same load reads



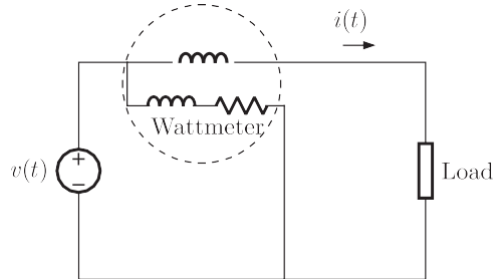
- (A) 4 V
- (B) 5 V
- (C) 8 V
- (D) 10 V

Q. 6

The bridge method commonly used for finding mutual inductance is

- (A) Heaviside Campbell bridge
- (B) Schering bridge
- (C) De Sauty bridge
- (D) Wien bridge

- Q. 7 For the circuit shown in the figure, the voltage and current expressions are  
 $v(t) = E_1 \sin(\omega t) + E_3 \sin(3\omega t)$  and  
 $i(t) = I_1 \sin(\omega t - \phi_1) + I_3 \sin(3\omega t - \phi_3) + I_5 \sin(5\omega t)$   
 The average power measured by the wattmeter is



- (A)  $\frac{1}{2} E_1 I_1 \cos \phi_1$  (B)  $\frac{1}{2} [E_1 I_1 \cos \phi_1 + E_3 I_3 \cos \phi_3 + E_5 I_5 \cos \phi_5]$   
 (C)  $\frac{1}{2} [E_1 I_1 \cos \phi_1 + E_3 I_3 \cos \phi_3]$  (D)  $\frac{1}{2} [E_1 I_1 \cos \phi_1 + E_3 I_1 \cos \phi_1]$

## YEAR 2012

TWO MARKS

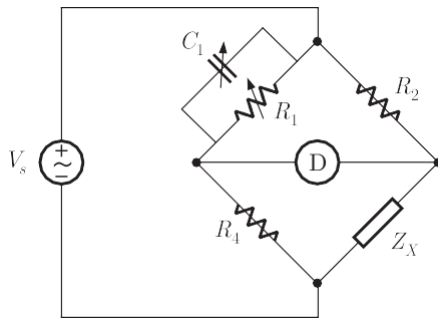
- Q. 8 An analog voltmeter uses external multiplier settings. With a multiplier setting of 20 kW, it reads 440 V and with a multiplier setting of 80 kW, it reads 352 V. For a multiplier setting of 40 kW, the voltmeter reads  
 (A) 371 V  
 (B) 383 V  
 (C) 394 V  
 (D) 406 V

## YEAR 2011

ONE MARK

- Q. 9 A dual trace oscilloscope is set to operate in the ALTERNATE mode. The control input of the multiplexer used in the y-circuit is fed with a signal having a frequency equal to  
 (A) the highest frequency that the multiplexer can operate properly  
 (B) twice the frequency of the time base (sweep) oscillator  
 (C) the frequency of the time base (sweep) oscillator  
 (D) half the frequency of the time base (sweep) oscillator
- Consider the following statement
- (1) The compensating coil of a low power factor wattmeter compensates the effect of the impedance of the current coil.  
 (2) The compensating coil of a low power factor wattmeter compensates the effect of the impedance of the voltage coil circuit.
- (A) (1) is true but (2) is false  
 (B) (1) is false but (2) is true  
 (C) both (1) and (2) are true  
 (D) both (1) and (2) are false

- Q. 10 The bridge circuit shown in the figure below is used for the measurement of an unknown element  $Z_X$ . The bridge circuit is best suited when  $Z_X$  is a



- (A) low resistance  
(B) high resistance  
(C) low  $Q$  inductor  
(D) lossy capacitor

YEAR 2011

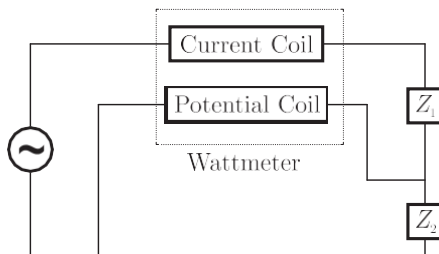
TWO MARKS

- Q. 11 A  $4\frac{1}{2}$  digit DMM has the error specification as: 0.2% of reading + 10 counts. If a dc voltage of 100 V is read on its 200 V full scale, the maximum error that can be expected in the reading is
- (A)  $\downarrow$  0.1%  
(B)  $\downarrow$  0.2%  
(C)  $\downarrow$  0.3%  
(D)  $\downarrow$  0.4%

YEAR 2010

ONE MARK

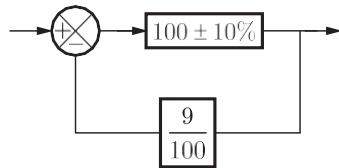
- Q. 12 A wattmeter is connected as shown in figure. The wattmeter reads.



- (A) Zero always  
(B) Total power consumed by  $Z_1$  and  $Z_2$   
(C) Power consumed by  $Z_1$   
(D) Power consumed by  $Z_2$
- Q. 13 An ammeter has a current range of 0-5 A, and its internal resistance is 0.2  $\Omega$ . In order to change the range to 0-25 A, we need to add a resistance of
- (A) 0.8  $\Omega$  in series with the meter  
(B) 1.0  $\Omega$  in series with the meter  
(C) 0.04  $\Omega$  in parallel with the meter  
(D) 0.05  $\Omega$  in parallel with the meter

Q. 14

As shown in the figure, a negative feedback system has an amplifier of gain 100 with  $\pm 10\%$  tolerance in the forward path, and an attenuator of value  $9/100$  in the feedback path. The overall system gain is approximately :



- (A) 10  $\pm$  1%  
(C) 10  $\pm$  5%

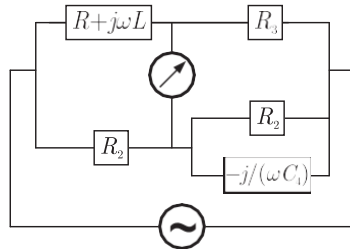
- (B) 10  $\pm$  2%  
(D) 10  $\pm$  10%

YEAR 2010

TWO MARKS

Q. 15

The Maxwell's bridge shown in the figure is at balance. The parameters of the inductive coil are.



- (A)  $R = R_2 R_3 / R_4, L = C_4 R_2 R_3$   
(B)  $L = R_2 R_3 / R_4, R = C_4 R_2 R_3$   
(C)  $R = R_4 / R_2 R_3, L = 1 / (C_4 R_2 R_3)$   
(D)  $L = R_4 / R_2 R_3, R = 1 / (C_4 R_2 R_3)$

YEAR 2009

ONE MARK

Q. 16

The pressure coil of a dynamometer type wattmeter is

- (A) Highly inductive  
(B) Highly resistive  
(C) Purely resistive  
(D) Purely inductive

Q. 17

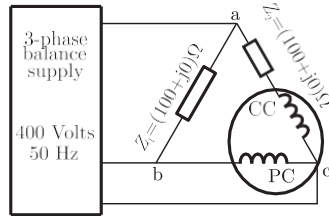
The two inputs of a CRO are fed with two stationary periodic signals. In the X-Y mode, the screen shows a figure which changes from ellipse to circle and back to ellipse with its major axis changing orientation slowly and repeatedly. The following inference can be made from this.

- (A) The signals are not sinusoidal  
(B) The amplitudes of the signals are very close but not equal  
(C) The signals are sinusoidal with their frequencies very close but not equal  
(D) There is a constant but small phase difference between the signals

YEAR 2009

TWO MARKS

- Q. 18 The figure shows a three-phase delta connected load supplied from a 400V, 50 Hz, 3-phase balanced source. The pressure coil (PC) and current coil (CC) of a wattmeter are connected to the load as shown, with the coil polarities suitably selected to ensure a positive deflection. The wattmeter reading will be



- (A) 0 (B) 1600 Watt  
 (C) 800 Watt (D) 400 Watt
- Q. 19 An average-reading digital multi-meter reads 10 V when fed with a triangular wave, symmetric about the time-axis. For the same input an rms-reading meter will read
- (A)  $\frac{20}{\sqrt{3}}$  (B)  $\frac{10}{3}$   
 (C)  $20\sqrt{3}$  (D)  $10\sqrt{3}$

YEAR 2008

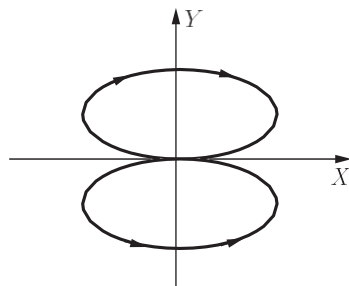
ONE MARK

- Q. 20 Two 8-bit ADCs, one of single slope integrating type and other of successive approximate type, take  $T_A$  and  $T_B$  times to convert 5 V analog input signal to equivalent digital output. If the input analog signal is reduced to 2.5 V, the approximate time taken by the two ADCs will respectively, be
- (A)  $T_A, T_B$  (B)  $T_A/2, T_B$   
 (C)  $T_A, T_B/2$  (D)  $T_A/2, T_B/2$

YEAR 2008

TWO MARKS

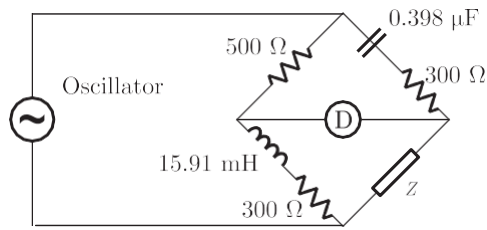
- Q. 21 Two sinusoidal signals  $p(w_1, t) = A \sin w_1 t$  and  $q(w_2 t)$  are applied to X and Y inputs of a dual channel CRO. The Lissajous figure displayed on the screen shown below :
- The signal  $q(w_2 t)$  will be represented as



- (A)  $q(w_2 t) = A \sin w_2 t, w_2 = 2w_1$  (B)  $q(w_2 t) = A \sin w_2 t, w_2 = w_1/2$   
 (C)  $q(w_2 t) = A \cos w_2 t, w_2 = 2w_1$  (D)  $q(w_2 t) = A \cos w_2 t, w_2 = w_1/2$

Q. 22

The ac bridge shown in the figure is used to measure the impedance  $Z$ .



kHz, then the impedance

If the bridge is balanced for oscillator frequency  $f = 2$

$Z$  will be

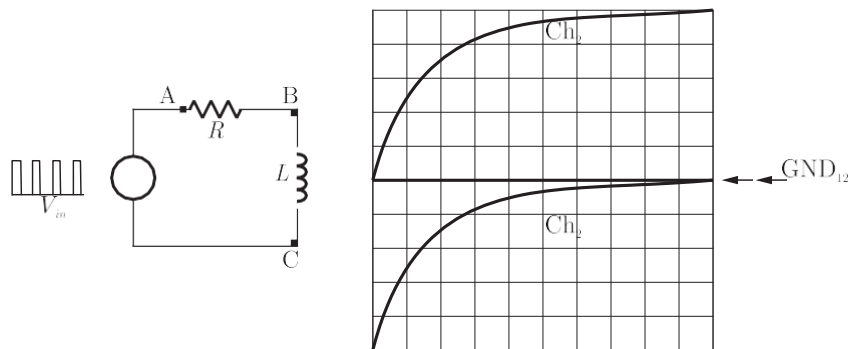
- (A)  $(260 + j0) \Omega$
- (B)  $(0 + j200) \Omega$
- (C)  $(260 - j200) \Omega$
- (D)  $(260 + j200) \Omega$

YEAR 2007

ONE MARK

Q. 23

The probes of a non-isolated, two channel oscilloscope are clipped to points A, B and C in the circuit of the adjacent figure.  $V_{in}$  is a square wave of a suitable low frequency. The display on Ch<sub>1</sub> and Ch<sub>2</sub> are as shown on the right. Then the “Signal” and “Ground” probes  $S_1, G_1$  and  $S_2, G_2$  of Ch<sub>1</sub> and Ch<sub>2</sub> respectively are connected to points :



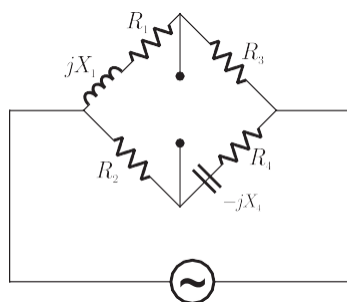
- (A) A, B, C, A
- (B) A, B, C, B
- (C) C, B, A, B
- (D) B, A, B, C

YEAR 2007

TWO MARKS

Q. 24

A bridge circuit is shown in the figure below. Which one of the sequence given below is most suitable for balancing the bridge ?



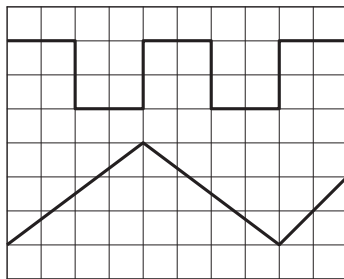
- (A) First adjust  $R_4$ , and then adjust  $R_1$
- (B) First adjust  $R_2$ , and then adjust  $R_3$
- (C) First adjust  $R_2$ , and then adjust  $R_4$
- (D) First adjust  $R_4$ , and then adjust  $R_2$

YEAR 2006

ONE MARK

Q. 25

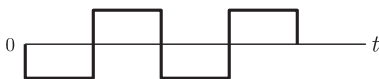
The time/div and voltage/div axes of an oscilloscope have been erased. A student connects a 1 kHz, 5 V p-p square wave calibration pulse to channel-1 of the scope and observes the screen to be as shown in the upper trace of the figure. An unknown signal is connected to channel-2 (lower trace) of the scope. If the time/div and V/div on both channels are the same, the amplitude (p-p) and period of the unknown signal are respectively



- (A) 5 V, 1 ms
- (B) 5 V, 2 ms
- (C) 7.5 V, 2 ms
- (D) 10 V, 1 ms

Q. 26

A sampling wattmeter (that computes power from simultaneously sampled values of voltage and current) is used to measure the average power of a load. The peak to peak voltage of the square wave is 10 V and the current is a triangular wave of 5 A p-p as shown in the figure. The period is 20 ms. The reading in W will be



- (A) 0 W
- (B) 25 W
- (C) 50 W
- (D) 100 W

YEAR 2006

TWO MARKS

Q. 27

A current of  $-8 + 6 \sqrt{2} (\sin wt + 30^\circ)$  A is passed through three meters. They are a centre zero PMMC meter, a true rms meter and a moving iron instrument. The respective reading (in A) will be

- (A) 8, 6, 10
- (B) 8, 6, 8
- (C) -8, 10, 10
- (D) -8, 2, 2



- Q. 28** A variable  $w$  is related to three other variables  $x, y, z$  as  $w = xy/z$ . The variables are measured with meters of accuracy  $\pm 0.5\%$  reading,  $\pm 1\%$  of full scale value and  $\pm 1.5\%$  reading. The actual readings of the three meters are 80, 20 and 50 with 100 being the full scale value for all three. The maximum uncertainty in the measurement of  $w$  will be
- (A)  $\pm 0.5\%$  rdg (B)  $\pm 5.5\%$  rdg  
(C)  $\pm 6.7\%$  rdg (D)  $\pm 7.0\%$  rdg
- Q. 29** A 200 / 1 Current transformer (CT) is wound with 200 turns on the secondary on a toroidal core. When it carries a current of 160 A on the primary, the ratio and phase errors of the CT are found to be  $-0.5\%$  and 30 minutes respectively. If the number of secondary turns is reduced by 1 new ratio-error(%) and phase-error(min) will be respectively
- (A) 0.0, 30 (B)  $-0.5, 35$   
(C)  $-1.0, 30$  (D)  $-1.0, 25$
- Q. 30**  $R_1$  and  $R_4$  are the opposite arms of a Wheatstone bridge as are  $R_3$  and  $R_2$ . The source voltage is applied across  $R_1$  and  $R_3$ . Under balanced conditions which one of the following is true
- (A)  $R_1 = R_3 R_4 / R_2$  (B)  $R_1 = R_2 R_3 / R_4$   
(C)  $R_1 = R_2 R_4 / R_3$  (D)  $R_1 = R_2 + R_3 + R_4$

**YEAR 2005****ONE MARK**

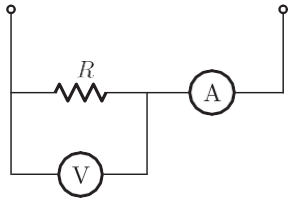
- Q. 31** The Q-meter works on the principle of
- (A) mutual inductance  
(B) self inductance  
(C) series resonance  
(D) parallel resonance
- Q. 32** A PMMC voltmeter is connected across a series combination of DC voltage source  $V_1 = 2$  V and AC voltage source  $V_2(t) = 3 \sin(4t)$  V. The meter reads
- (A) 2 V (B) 5 V  
(C)  $(2 + 3/2)$  V (D)  $(17/2)$  V
- Q. 33** A digital-to-analog converter with a full-scale output voltage of 3.5 V has a resolution close to 14 mV. Its bit size is
- (A) 4 (B) 8  
(C) 16 (D) 32

**YEAR 2005****TWO MARKS**

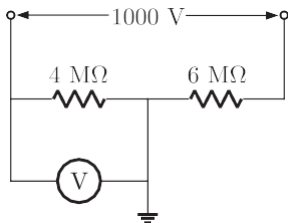
- Q. 34** The simultaneous application of signals  $x(t)$  and  $y(t)$  to the horizontal and vertical plates, respectively, of an oscilloscope, produces a vertical figure-of-8 display. If P and Q are constants and  $x(t) = P \sin(4t + 30^\circ)$ , then  $y(t)$  is equal to
- (A)  $Q \sin(4t - 30^\circ)$  (B)  $Q \sin(2t + 15^\circ)$   
(C)  $Q \sin(8t + 60^\circ)$  (D)  $Q \sin(4t + 30^\circ)$

- Q. 35** A DC ammeter has a resistance of  $0.1 \Omega$  and its current range is  $0-100 \text{ A}$ . If the range is to be extended to  $0-500 \text{ A}$ , then meter required the following shunt resistance
- (A)  $0.010 \Omega$  (B)  $0.011 \Omega$   
(C)  $0.025 \Omega$  (D)  $1.0 \Omega$

- Q. 36** The set-up in the figure is used to measure resistance  $R$ . The ammeter and voltmeter resistances are  $0.01 \Omega$  and  $2000 \Omega$ , respectively. Their readings are  $2 \text{ A}$  and  $180 \text{ V}$ , respectively, giving a measured resistance of  $90 \Omega$ . The percentage error in the measurement is



- (A) 2.25% (B) 2.35%  
(C) 4.5% (D) 4.71%
- Q. 37** A  $1000 \text{ V}$  DC supply has two 1-core cables as its positive and negative leads: their insulation resistances to earth are  $4 \text{ M}\Omega$  and  $6 \text{ M}\Omega$ , respectively, as shown in the figure. A voltmeter with resistance  $50 \text{ k}\Omega$  is used to measure the insulation of the cable. When connected between the positive core and earth, then voltmeter reads



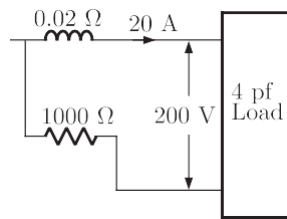
- (A)  $8 \text{ V}$  (B)  $16 \text{ V}$   
(C)  $24 \text{ V}$  (D)  $40 \text{ V}$
- Q. 38** Two wattmeters, which are connected to measure the total power on a three-phase system supplying a balanced load, read  $10.5 \text{ kW}$  and  $-2.5 \text{ kW}$ , respectively. The total power and the power factor, respectively, are
- (A)  $13.0 \text{ kW}$ ,  $0.334$   
(B)  $13.0 \text{ kW}$ ,  $0.684$   
(C)  $8.0 \text{ kW}$ ,  $0.52$   
(D)  $8.0 \text{ kW}$ ,  $0.334$

## YEAR 2004

## ONE MARK

- Q. 39** A dc potentiometer is designed to measure up to about  $2 \text{ V}$  with a slide wire of  $800 \text{ mm}$ . A standard cell of emf  $1.18 \text{ V}$  obtains balance at  $600 \text{ mm}$ . A test cell is seen to obtain balance at  $680 \text{ mm}$ . The emf of the test cell is
- (A)  $1.00 \text{ V}$  (B)  $1.34 \text{ V}$   
(C)  $1.50 \text{ V}$  (D)  $1.70 \text{ V}$

- Q. 40** The circuit in figure is used to measure the power consumed by the load. The current coil and the voltage coil of the wattmeter have  $0.02 \Omega$  and  $1000 \Omega$  resistances respectively. The measured power compared to the load power will be

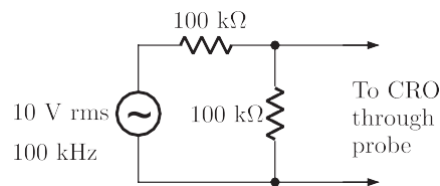


- (A) 0.4 % less  
(B) 0.2% less  
(C) 0.2% more  
(D) 0.4% more
- Q. 41** A galvanometer with a full scale current of  $10 \text{ mA}$  has a resistance of  $1000 \Omega$ . The multiplying power (the ratio of measured current to galvanometer current) of  $100 \Omega$  shunt with this galvanometer is
- (A) 110  
(B) 100  
(C) 11  
(D) 10

## YEAR 2004

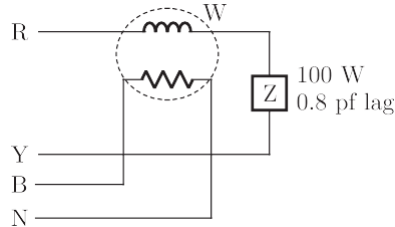
## TWO MARKS

- Q. 42** A CRO probe has an impedance of  $500 \text{ k}\Omega$  in parallel with a capacitance of  $10 \text{ pF}$ . The probe is used to measure the voltage between P and Q as shown in figure. The measured voltage will be



- (A) 3.53 V  
(B) 4.37 V  
(C) 4.54 V  
(D) 5.00 V
- Q. 43** A moving coil of a meter has 100 turns, and a length and depth of  $10 \text{ mm}$  and  $20 \text{ mm}$  respectively. It is positioned in a uniform radial flux density of  $200 \text{ mT}$ . The coil carries a current of  $50 \text{ mA}$ . The torque on the coil is
- (A)  $200 \text{ mNm}$   
(B)  $100 \text{ mNm}$   
(C)  $2 \text{ mNm}$   
(D)  $1 \text{ mNm}$
- Q. 44** A dc A-h meter is rated for  $15 \text{ A}$ ,  $250 \text{ V}$ . The meter constant is  $14.4 \text{ A-sec/rev}$ . The meter constant at rated voltage may be expressed as
- (A)  $3750 \text{ rev/kWh}$   
(B)  $3600 \text{ rev / kWh}$   
(C)  $1000 \text{ rev/kWh}$   
(D)  $960 \text{ rev / kWh}$
- Q. 45** A moving iron ammeter produces a full scale torque of  $240 \text{ mNm}$  with a deflection of  $120^\circ$  at a current of  $10 \text{ A}$ . The rate of change of self induction ( $\text{mH / radian}$ ) of the instrument at full scale is
- (A)  $2.0 \text{ mH / radian}$   
(B)  $4.8 \text{ mH / radian}$   
(C)  $12.0 \text{ mH / radian}$   
(D)  $114.6 \text{ mH / radian}$

- Q. 46** A single-phase load is connected between R and Y terminals of a 415 V, symmetrical, 3-phase, 4-wire system with phase sequence RYB. A wattmeter is connected in the system as shown in figure. The power factor of the load is 0.8 lagging. The wattmeter will read



- (A)  $-795 \text{ W}$  (B)  $-597 \text{ W}$   
 (C)  $+597 \text{ W}$  (D)  $+795 \text{ W}$
- Q. 47** A 50 Hz, bar primary CT has a secondary with 500 turns. The secondary supplies 5 A current into a purely resistive burden of 1 W. The magnetizing ampere-turns is 200. The phase angle between the primary and second current is
- (A) 4.6c (B) 85.4c  
 (C) 94.6c (D) 175.4c
- Q. 48** The core flux in the CT of Prob Q.44, under the given operating conditions is
- (A) 0 (B) 45.0 mWb  
 (C) 22.5 mWb (D) 100.0 mWb

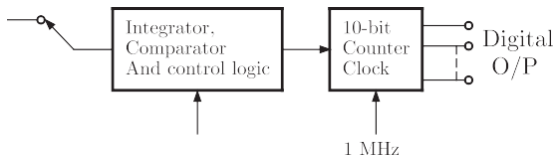
**YEAR 2003****ONE MARK**

- Q. 49** A Manganin swap resistance is connected in series with a moving coil ammeter consisting of a milli-ammeter and a suitable shunt in order to
- (A) minimise the effect of temperature variation  
 (B) obtain large deflecting torque  
 (C) reduce the size of the meter  
 (D) minimise the effect of stray magnetic fields
- Q. 50** The effect of stray magnetic field on the actuating torque of a portable instrument is maximum when the operating field of the instrument and the stray fields are
- (A) perpendicular  
 (B) parallel  
 (C) inclined at  $60^\circ$   
 (D) inclined at  $30^\circ$
- Q. 51** A reading of 120 is obtained when standard inductor was connected in the circuit of a Q-meter and the variable capacitor is adjusted to value of 300 pF. A lossless capacitor of unknown value  $C_x$  is then connected in parallel with the variable capacitor and the same reading was obtained when the variable capacitor is readjusted to a value of 200 pF. The value of  $C_x$  in pF is
- (A) 100 (B) 200  
 (C) 300 (D) 500

YEAR 2003

TWO MARKS

- Q. 52** The simplified block diagram of a 10-bit A / D converter of dual slope integrator type is shown in figure. The 10-bit counter at the output is clocked by a 1 MHz clock. Assuming negligible timing overhead for the control logic, the maximum frequency of the analog signal that can be converted using this A / D converter is approximately



- (A) 2 kHz (B) 1 kHz  
(C) 500 Hz (D) 250 Hz

- Q. 53** The items in Group-I represent the various types of measurements to be made with a reasonable accuracy using a suitable bridge. The items in Group-II represent the various bridges available for this purpose. Select the correct choice of the item in Group-II for the corresponding item in Group-I from the following

**List-I**

- P.** Resistance in the milli-ohm range  
**Q.** Low values of Capacitance  
**R.** Comparison of resistance which are nearly equal  
**S.** Inductance of a coil with a large time-constant

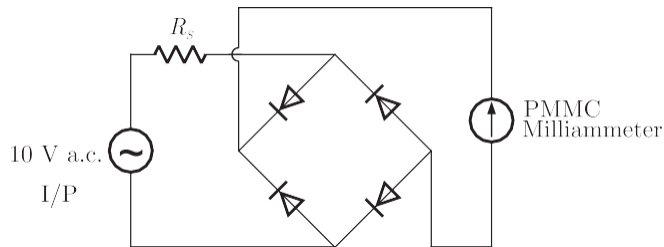
**List-II**

1. Wheatstone Bridge
2. Kelvin Double Bridge
3. Schering Bridge
4. Wien's Bridge
5. Hay's Bridge
6. Carey-Foster Bridge

**Codes :**

- (A) P=2, Q=3, R=6, S=5 (B) P=2, Q=6, R=4, S=5  
(C) P = 2, Q = 3, R = 5, S=4 (D) P=1, Q=3, R=2, S=6

- Q. 54** A rectifier type ac voltmeter of a series resistance  $R_s$ , an ideal full-wave rectifier bridge and a PMMC instrument as shown in figure. The internal resistance of the instrument is  $100 \Omega$  and a full scale deflection is produced by a dc current of 1 mA. The value of  $R_s$  required to obtain full scale deflection with an ac voltage of 100 V (rms) applied to the input terminals is



- (A) 63.56  $\Omega$  (B) 69.93  $\Omega$   
(C) 89.93  $\Omega$  (D) 141.3 k $\Omega$

- Q. 55** A wattmeter reads 400 W when its current coil is connected in the R-phase and its pressure coil is connected between this phase and the neutral of a symmetrical 3-phase system supplying a balanced star connected 0.8 p.f. inductive load. This phase sequence is RYB. What will be the reading of this wattmeter if its pressure coil alone is reconnected between the B and Y phases, all other connections

remaining as before ?

- (A) 400.0
- (B) 519.6
- (C) 300.0
- (D) 692.8

**Q. 56** The inductance of a certain moving-iron ammeter is expressed as  $L = 10 + 3q - (q^2 / 4) \text{ mH}$ , where  $q$  is the deflection in radians from the zero position. The control spring torque is  $25 \times 10^{-6} \text{ Nm / radian}$ . The deflection of the pointer in radian when the meter carries a current of 5 A, is

- (A) 2.4
- (B) 2.0
- (C) 1.2
- (D) 1.0

**Q. 57** A 500A / 5A, 50 Hz transformer has a bar primary. The secondary burden is a pure resistance of 1 W and it draws a current of 5 A. If the magnetic core requires 250 AT for magnetization, the percentage ratio error is

- (A) 10.56
- (B) -10.56
- (C) 11.80
- (D) -11.80

**Q. 58** The voltage-flux adjustment of a certain 1-phase 220 V induction watt-hour meter is altered so that the phase angle between the applied voltage and the flux due to it is  $85^\circ$  (instead of  $90^\circ$ ). The errors introduced in the reading of this meter when the current is 5 A at power factor of unity and 0.5 lagging are respectively

- (A) 3.8 mW, 77.4 mW
- (B) -3.8 mW, -77.4 mW
- (C) -4.2 W, -85.1 W
- (D) 4.2 W, 85.1 W

**Q. 59** Group-I represents the figures obtained on a CRO screen when the voltage signals  $V_x = V_{xm} \sin \omega t$  and  $V_y = V_{ym} \sin(\omega t + F)$  are given to its X and Y plates respectively and  $F$  is changed. Choose the correct value of  $F$  from Group-I to match with the corresponding figure of Group-II.

Group-I

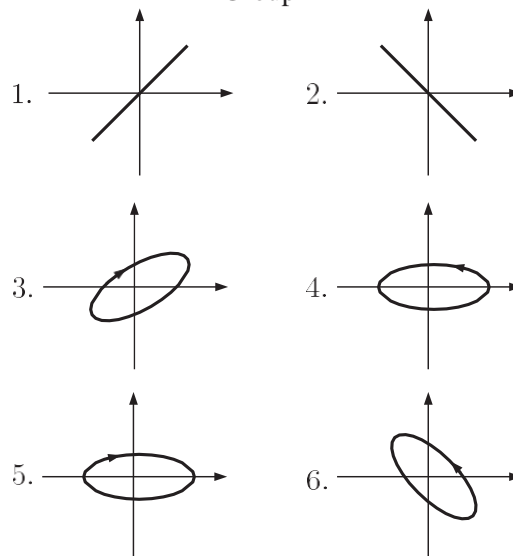
P.  $F = 0$

Q.  $F = \pi/2$

R.  $\pi < F < 3\pi/2$

S.  $F = 3\pi/2$

Group-II



**Codes :**

- (A) P = 1, Q = 3, R = 6, S = 5
- (B) P = 2, Q = 6, R = 4, S = 5
- (C) P = 2, Q = 3, R = 5, S = 4
- (D) P = 1, Q = 5, R = 6, S = 4

\*\*\*\*\*

# SOLUTIONS

**Sol. 1**

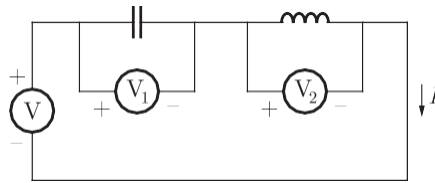
Option (B) is correct.

For an ideal voltmeter internal resistance is always zero. So we can apply the KVL along the two voltmeters as

$$V - V_1 - V_2 = 0$$

or

$$V = V_1 + V_2$$



**Sol. 2**

Option (A) is correct.

For the +ve half cycle of  $I/p$  voltage, diode will be forward biased ( $V_g = 0$ , ideal diode) Therefore, the voltmeter will be short circuited and reads

$$V_1 = 0 \text{ volt} \quad (\text{for + ve half cycle})$$

Now, for -ve half cycle, diode will be reverse biased and treated as open circuit. So, the voltmeter reads the voltage across  $100 \text{ kW}$ . Which is given by

$$V_2 = 100 \# \frac{14.14 \text{ Oc}}{100 + 1}$$

So, 
$$V_{2, rms} = \frac{14}{\sqrt{2}} \text{ volt}$$

Therefore, the average voltage for the whole time period is obtained as

$$\begin{aligned} V_{ave} &= \frac{V_1 + V_{2, rms}}{2} = \frac{0 + 14 \times \frac{2}{2\sqrt{2}}}{2} = \frac{14}{2\sqrt{2}} \\ &= 4.94 \approx 4.46 \text{ volt} \end{aligned}$$

**Sol. 3**

Option (C) is correct.

The quality factor of the inductances are given by

$$q_1 = \frac{\omega L_1}{R_1}$$

and

$$q_2 = \frac{\omega L_2}{R_2}$$

So, in series circuit, the effective quality factor is given by

$$\begin{aligned} Q &= \frac{|X_{Leq}|}{R_{eq}} = \frac{\omega L_1 + \omega L_2}{R_1 + R_2} \\ &= \frac{\frac{\omega L_1}{R_1} R_2 + \frac{\omega L_2}{R_2} R_1}{R_2 + R_1} = \frac{q_1 R_2 + q_2 R_1}{R_1 + R_2} \end{aligned}$$

**Sol. 4**

Option (C) is correct.

**Sol. 5**

Option (A) is correct.

PMDC instrument reads average (dc) value.

$$\begin{aligned}
 V_{avg} &= \frac{1}{T} \int_0^T v(t) dt = \frac{1}{20 \times 10^{-3}} \int_0^{20} v(t) dt \\
 &= \frac{1}{20} \left[ \int_0^{10} t dt + \int_{10}^{12} (-5) dt + \int_{12}^{20} 5 dt \right] \\
 &= \frac{1}{20} \left[ \frac{t^2}{2} \Big|_0^{10} - 5t \Big|_{10}^{12} + 5t \Big|_{12}^{20} \right] \\
 &= \frac{1}{20} [50 - 5(2) + 5(8)] = \frac{80}{20} = 4 \text{ V}
 \end{aligned}$$

Sol. 6 Option (A) is correct.

Heaviside mutual inductance bridge measures mutual inductance in terms of a known self-inductance.

Sol. 7 Option (C) is correct.

Let  $\omega t = q$ , we have instantaneous voltage and current as follows.

$$v(t) = E_1 \sin q + E_3 \sin 3q$$

$$i(t) = I_1 \sin(q - \phi_1) + I_3 \sin(3q - \phi_3) + I_5 \sin(5q)$$

We know that wattmeter reads the average power, which is given as

$$P = \frac{1}{2\pi} \int_0^{2\pi} v(t) i(t) dq \quad \dots(i)$$

We can solve this integration using following results.

$$(i) \frac{1}{2\pi} \int_0^{2\pi} A \sin(q + a) \cdot B \sin(q + b) dq = \frac{1}{2} AB \cos(a - b)$$

$$(ii) \frac{1}{2\pi} \int_0^{2\pi} A \sin(q + a) \cdot B \cos(q + a) dq = \frac{1}{2} AB \sin(a - b)$$

$$(iii) \frac{1}{2\pi} \int_0^{2\pi} A \sin(mq + a) \cdot B \cos(nq + b) dq = 0$$

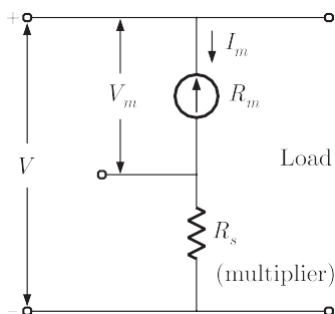
$$(iv) \frac{1}{2\pi} \int_0^{2\pi} A \sin(mq + a) \cdot B \sin(nq + b) dq = 0$$

Result (iii) and (iv) implies that power is transferred between same harmonics of voltages and currents. Thus integration of equation (i) gives.

$$P = \frac{1}{2} E_1 I_1 \cos \phi + \frac{1}{2} E_3 I_3 \cos \phi_3$$

Sol. 8 Option (D) is correct.

A voltmeter with a multiplier is shown in figure below.



Here

$I_m$  = Fully scale deflection current of meter.

$R_m$  = Internal resistance of meter

$R_s$  = Voltage across the meter

$V$  = Full range voltage of instrument

$V_m = I_m R_m$



$$V = I_m (R_m + R_s)$$

$$\frac{V}{V_m} = \frac{R_m + R_s}{R_m} = 1 + \frac{R_s}{R_m}$$

Here when,  
So,

$$\frac{R_{s1}}{V} = \frac{20 \text{ kW}}{440} = \frac{V_{m1}}{440} = 1 + \frac{20 \text{ k}}{R_m} \quad \dots(i)$$

When,  
So,

$$\frac{R_{s2}}{V} = \frac{80 \text{ kW}}{352} = \frac{V_{m2}}{352} = 1 + \frac{80 \text{ k}}{R_m} \quad \dots(ii)$$

Solving equation (i) and (ii), we get

$$V = 480 \text{ V}, R_m = 220 \text{ kW}$$

So when

$$R_{s3} = 40 \text{ kW}, V_{m3} = ?$$

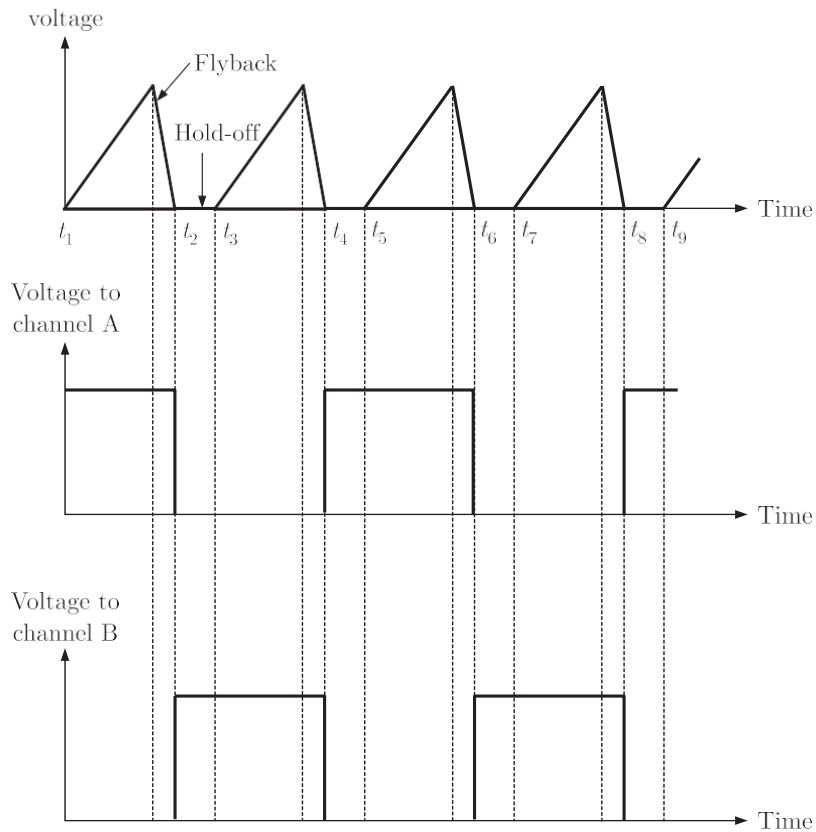
$$\frac{480}{V_{m3}} = 1 + \frac{40 \text{ k}}{220 \text{ k}} \quad \& \quad V_{m3} = 406 \text{ V}$$

Sol. 9

Option (C) is correct.

In the alternate mode it switches between channel A and channel B, letting each through for one cycle of horizontal sweep as shown in the figure.

horizontal sweep



Sol. 10

Option (A) is correct.

The compensating coil compensation the effect of impedance of current coil.

Sol. 11

Option (C) is correct.

Let

so admittance

$$Z_1 = R_1 \parallel j\omega C_1$$

$$Y_1 = \frac{1}{Z_1} = \frac{1}{R_1} + j\omega C_1$$

$$Z_2 = R_2 \quad \text{and} \quad Z_4 = R_4$$

Let  $Z_X = R_X + j\omega L_X$  (Unknown impedance)

For current balance condition of the Bridge

$$Z_2 Z_4 = Z_X Z_1 = \frac{Z_X}{Y_1}$$

Let  $Z_X = Z_2 Z_4 Y_1$

$$R_X + j\omega L_X = R_2 R_4 \frac{1}{R} + j\omega C_1$$

Equating imaginary and real parts

$$R_X = \frac{R_2 R_4}{R_1} \quad \text{and} \quad L_X = R_2 R_4 C_1$$

Quality factor of inductance which is being measured

$$Q = \frac{\omega L_X}{R_X} = \omega R_1 C_1$$

From above equation we can see that for measuring high values of  $Q$  we need a large value of resistance  $R_4$  which is not suitable. This bridge is used for measuring low  $Q$  coils.

*Note:* We can observe directly that this is a maxwell's bridge which is suitable for low values of  $Q$  (i.e.  $Q < 10$ )

**Sol. 12** Option (C) is correct.

$4 \frac{1}{2}$  digit display will read from 000.00 to 199.99 So error of 10 counts is equal to =  $\pm 0.10$  V

For 100 V, the maximum error is

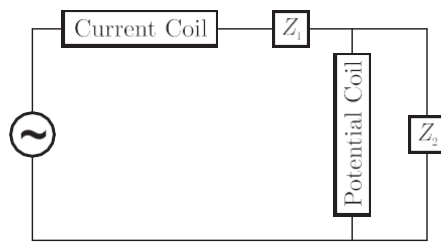
$$e = \pm (100 \times 0.002 + 0.1) = \pm 0.3 \text{ V}$$

Percentage error

$$= \pm \frac{0.3 \times 100}{100} \% = \pm 0.3 \% \text{ of reading}$$

**Sol. 13** Option (D) is correct.

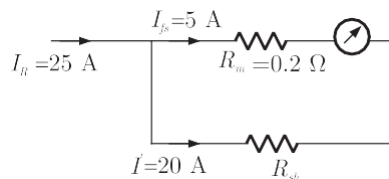
Since potential coil is applied across  $Z_2$  as shown below



Wattmeter read power consumed by  $Z_2$

**Sol. 14** Option (D) is correct.

Given that full scale current is 5 A



$$\text{Current in shunt } I_1 = I_R - I_{fs} = 25 - 5 = 20 \text{ A}$$

$$20 \times R_{sh} = 5 \times 0.2$$

$$R_{sh} = \frac{1}{20} = .05 \text{ W}$$

Sol. 15

Option (A) is correct.

Overall gain of the system is

$$g = \frac{100}{1 + 100 \frac{9}{100}} = 10 \text{ (zero error)}$$

Gain with error

$$g = \frac{100 + 10\%}{1 + (100 + 10\%) \frac{9}{100}} = \frac{110}{1 + \frac{110 \cdot 9}{100}} = 10.091$$

$$\text{error } \Delta g = 10.091 - 10 = 0.1$$

Similarly

$$g = \frac{100 - 10\%}{1 + (100 - 10\%) \frac{9}{100}} = \frac{90}{1 + \frac{90 \cdot 9}{100}} = 9.89$$

$$\text{error } \Delta g = 9.89 - 10 = -0.1$$

$$\text{So gain } g = 10 \pm 0.1 = 10 \pm 1\%$$

Sol. 16

Option (A) is correct.

At balance condition

$$(R + j\omega L) C R_4 < \frac{-j}{\omega C} m = R_2 R_3$$

$$(R + j\omega L) \frac{-jR_4}{\omega C_4} = R_2 R_3$$

$$C R_4 - \frac{j}{\omega C} m$$

$$\frac{-jR R_4}{\omega C_4} + \frac{\omega L R_4}{\omega C_4} = R_2 R_3 R_4 - \frac{jR_2 R_3}{\omega C_4}$$

$$\frac{-jR R_4}{\omega C_4} + \frac{L R_4}{C_4} = R_2 R_3 R_4 - \frac{jR_2 R_3}{\omega C_4}$$

Comparing real &amp; imaginary parts.

$$\frac{R R_4}{\omega C_4} = \frac{R_2 R_3}{\omega C_4}$$

$$R = \frac{R_2 R_3}{R_4}$$

Similarly,

$$\frac{L R_4}{C_4} = R_2 R_3 R_4$$

$$L = R_2 R_3 C_4$$

Sol. 17

Option (B) is correct.

Since Potential coil is connected across the load terminal, so it should be highly resistive, so that all the voltage appears across load.

Sol. 18

Option (D) is correct.

A circle is produced when there is a 90° phase difference between vertical and horizontal inputs.

Sol. 19

Option (C) is correct.

$$\text{Wattmeter reading } P = V_{PC} I_{CC}$$

$V_{PC}$  " Voltage across potential coil.

$I_{CC}$  " Current in current coil.

$$V_{PC} = V_{bc} = 400 + -120c$$

$$I_{CC} = I_{ac} = \frac{400 + 120c}{100} = 4 + 120c$$

Power  $P = 400 + -120c \neq 4 + 120c$   
 $= 1600 + 240c = 1600 \neq \frac{1}{2} = 800 \text{ Watt}$

Sol. 20 Option (D) is correct.

Average value of a triangular wave

$$V_{av} = \frac{V_m}{3}$$

rms value  $V_{ms} = \frac{V_m}{\sqrt{3}}$

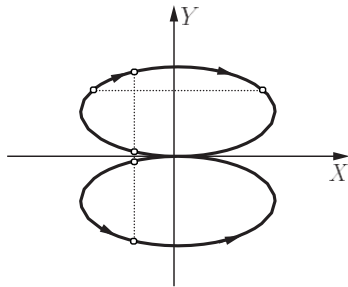
Given that  $V_{av} = \frac{V_m}{3} = 10 \text{ V}$

So  $V_{rms} = \frac{V_m}{\sqrt{3}} = \sqrt{3} V_{av} = 10\sqrt{3} \text{ V}$

Sol. 21 Option (A) is correct.

Conversion time does not depend on input voltage so it remains same for both type of ADCs.

Sol. 22 Option (D) is correct.



Frequency ratio  $\frac{f_Y}{f_X} = \frac{\text{meeting points of horizontal tangents}}{\text{meeting points of vertical tangents}}$

$$\frac{f_Y}{f_X} = \frac{2}{4}$$

$$f_Y = \frac{1}{2}(f_X)$$

$$\omega_2 = \omega_1 / 2$$

Since the Lissajous figures are ellipse, so there is a phase difference of  $90^\circ$  exists between vertical and horizontal inputs.

So  $q(\omega_2 t) = A \cos \omega_2 t, \omega_2 = \omega_1 / 2$

Sol. 23 Option (A) is correct.

Impedance of different branches is given as

$$Z_{AB} = 500 \text{ W}$$

$$Z_{BC} = \frac{1}{j \neq 2\text{p} \neq 2 \neq 10 \neq 0.398 \text{ mF}} + 300 \text{ W}$$

$$= (-200j + 300) \text{ W}$$

$$Z_{AD} = j \neq 2\text{p} \neq 2 \neq 10^3 \neq 15.91 \text{ mH} + 300 \text{ W}$$

$$= (200j + 300) \text{ W}$$

To balance the bridge

$$Z_{AB} Z_{CD} = Z_{AD} Z_{BC}$$

$$500Z = (200j + 300)(-200j + 300)$$

$$500Z = 130000$$

$$Z = (260 + j0) \Omega$$

**Sol. 24** Option (B) is correct.

Since both the waveform appeared across resistor and inductor are same so the common point is B. Signal Probe  $S_1$  is connecte with A,  $S_2$  is connected with C and both the ground probes  $G_1$  and  $G_2$  are connected with common point B.

**Sol. 25** Option (A) is correct.

To balance the bridge

$$(R_1 + jX_1)(R_4 - jX_4) = R_2R_3$$

$$(R_1R_4 + X_1X_4) + j(X_1R_4 - R_1X_4) = R_2R_3$$

comparing real and imaginary parts on both sides of equations

$$R_1R_4 + X_1X_4 = R_2R_3 \quad \dots(1)$$

$$X_1R_4 - R_1X_4 = 0 \ \& \ \frac{X_1}{R_4} = \frac{R_1}{R_4} \quad \dots(2)$$

from eq(1) and (2) it is clear that for balancing the bridge first balance  $R_4$  and then  $R_1$ .

**Sol. 26** Option (C) is correct.

From the Calibration pulse we can obtain

$$\frac{\text{Voltage}}{\text{Division}} (3 \text{ V}) = \frac{5}{2} = 2.5 \text{ V}$$

$$\frac{\text{Time}}{\text{Division}} (3 \text{ T}) = \frac{1 \text{ ms}}{4} = \frac{1}{4} \text{ msec}$$

So amplitude (p-p) of unknown signal is

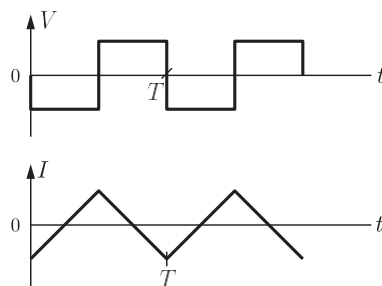
$$V_{P-P} = 3 \text{ V} \# 5 = 2.5 \# 5 = 7.5 \text{ V}$$

$$\text{Time period } T = 3 \text{ T} \# 8 = \frac{1}{4} \# 8 = 2 \text{ ms}$$

**Sol. 27** Option (A) is correct.

Reading of wattmeter (Power) in the circuit

$$P_{av} = \frac{1}{T_0} \int V I dt = \text{Common are between } V - I$$



total common area = 0 ( Positive and negative area are equal)

So  $P_{av} = 0$

**Sol. 28** Option (C) is correct.

PMMC instrument reads only dc value so

$$I_{PMMC} = -8 \text{ A}$$

rms meter reads rms value so

$$I_{rms} = \sqrt{(-8)^2 + \frac{(6\sqrt{2})^2}{2}} = \sqrt{64 + 36} = 10 \text{ A}$$

Moving iron instrument also reads rms value of current So

$$I_{MI} = 10 \text{ mA}$$

Reading are  $(I_{PMMC}, I_{rms}, I_{MI}) = (-8 \text{ A}, 10 \text{ A}, 10 \text{ A})$

Sol. 29

Option (D) is correct.

$$\text{Given that } w = \frac{xy}{z}$$

$$\log w = \log x + \log y - \log z$$

Maximum error in w

$$\% \frac{dw}{w} = \% \frac{dx}{x} + \% \frac{dy}{y} + \% \frac{dz}{z}$$

$$\frac{dx}{x} = \% 0.5\% \text{ reading}$$

$$\frac{dy}{y} = \% 1\% \text{ full scale} = \% \frac{1}{100} \# 100 = \% 1$$

$$\frac{dy}{y} = \% \frac{1}{20} \# 100 = \% 5\% \text{ reading}$$

$$\frac{dz}{z} = 1.5\% \text{ reading}$$

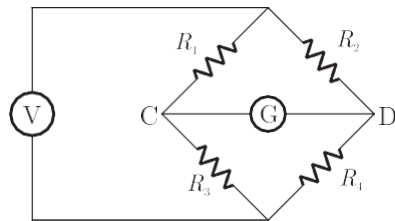
$$\text{So } \% \frac{dw}{w} = \% 0.5\% + \% 5\% + \% 1.5\% = \% 7\%$$

Sol. 30

Option ( ) is correct.

Sol. 31

Option (B) is correct.



In balanced condition there is no current in CD arm so  $V_C = V_D$

Writing node equation at C and D

$$\frac{V_C - V}{R} + \frac{V_C}{R_3} = 0 \ \& \ V_C = V \frac{R_3}{R_1 + R_3} I$$

$$\frac{V_D - V}{R} + \frac{V_D}{R_4} = 0 \ \& \ V_D = V \frac{R_4}{R_2 + R_4} I$$

$$\text{So } V \frac{R_3}{R_1 + R_3} I = V \frac{R_4}{R_2 + R_4} I$$

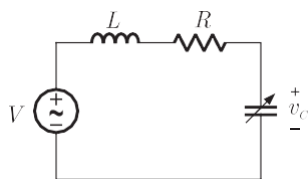
$$R_2 R_3 + R_3 R_4 = R_1 R_4 + R_3 R_4$$

$$R_1 = R_2 R_3 / R_4$$

Sol. 32

Option (C) is correct.

Q-meter works on the principle of series resonance.



At resonance  $V_C = V_L$

$$\text{and } I = \frac{V}{R}$$

$$\text{Quality factor } Q = \frac{\omega L}{R} = \frac{1}{\omega CR} = \frac{\omega L \cdot I}{R \cdot I} = \frac{V_L}{E} = \frac{V_C}{E}$$

Thus, we can obtain Q

Sol. 33

Option (A) is correct.

PMMC instruments reads DC value only so it reads 2 V.

Sol. 34

Option (B) is correct.

$$\text{Resolution of n-bit DAC} = \frac{V_{fs}}{2^n - 1}$$

$$\text{So } 14 \text{ mV} = \frac{3.5 \text{ V}}{2^n - 1}$$

$$2^n - 1 = \frac{3.5}{14 \times 10^{-3}}$$

$$2^n - 1 = 250$$

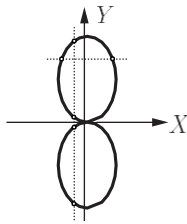
$$2^n = 251$$

$$n = 8 \text{ bit}$$

Sol. 35

Option (B) is correct.

We can obtain the frequency ratio as following



$$\frac{f_Y}{f_X} = \frac{\text{meeting points of horizontal tangents}}{\text{meeting points of vertical tangents}}$$

$$\frac{f_Y}{f_X} = \frac{2}{4}$$

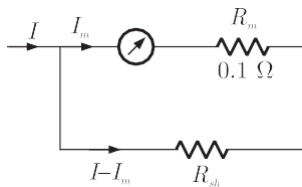
$$f_Y = \frac{1}{2} f_X$$

There should exist a phase difference (15c) also to produce exact figure of-8.

Sol. 36

Option (C) is correct.

The configuration is shown below



It is given that  $I_m = 100 \text{ A}$

Range is to be extended to  $0 - 500 \text{ A}$ ,

$$I = 500 \text{ A}$$

So

$$I_m R_m = (I - I_m) R_{sh}$$

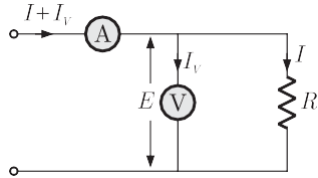
$$100 \times 0.1 = (500 - 100) R_{sh}$$

$$R_{sh} = \frac{100 \times 0.1}{400} = 0.025 \text{ W}$$

Sol. 37

Option (D) is correct.

The configuration is shown below



Current in voltmeter is given by

$$I_V = \frac{E}{2000} = \frac{180}{2000} = .09 \text{ A}$$

$$I + I_V = 2 \text{ amp}$$

So

$$I = 2 - .09 = 1.91 \text{ V}$$

$$R = \frac{E}{I} = \frac{180}{1.91} = 94.24 \text{ W}$$

Ideally

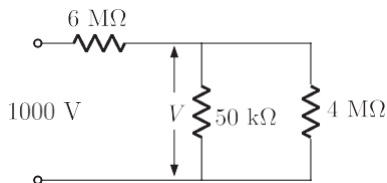
$$R_0 = \frac{180}{2} = 90 \text{ W}$$

$$\% \text{ error} = \frac{R - R_0}{R_0} \times 100 = \frac{94.24 - 90}{90} \times 100 = 4.71\%$$

Sol. 38

Option (A) is correct.

The measurement system is shown below



Voltmeter reading

$$V = \frac{1000}{\frac{6 \text{ MW}}{50 \text{ kW}} + \frac{4 \text{ MW}}{50 \text{ kW}}} = \frac{1000}{6 + .049} = 8.10 \text{ V}$$

Sol. 39

Option (D) is correct.

$$\text{Total power } P = P_1 + P_2 = 10.5 - 2.5 = 8 \text{ kW}$$

$$\text{Power factor} = \cos \phi$$

Where

$$\phi = \tan^{-1} \left( \sqrt{3} \frac{P_2 - P_1}{P_2 + P_1} \right) = \tan^{-1} \left( \sqrt{3} \times \frac{-13}{8} \right) = -70.43^\circ$$

$$\text{Power factor} = \cos \phi = 0.334$$

Sol. 40

Option (B) is correct.

for the dc potentiometer  $E \propto l$

$$\text{so, } \frac{E_1}{E_2} = \frac{l_1}{l_2}$$

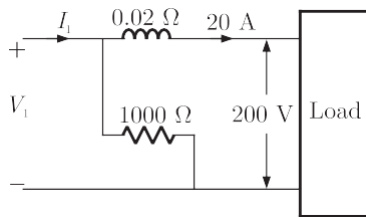
$$E_2 = E_1 \frac{l_1}{l_2} = (1.18) \times \frac{680}{600} = 1.34 \text{ V}$$



Sol. 41

Option (C) is correct.

Let the actual voltage and current are  $I_1$  and  $V_1$  respectively, then



Current in CC is 20 A

$$20 = I_1 \frac{1000}{1000 + 0.02}$$

$$I_1 = 20.0004 \text{ A} \approx 20 \text{ A}$$

$$200 = V_1 - 0.02 \times 20 = 200.40$$

$$\text{Power measured } P_m = V_1 I_1 = 20 (200.40) = 4008 \text{ W}$$

Load power

$$P_L = 20 \times 200 = 4000 \text{ W}$$

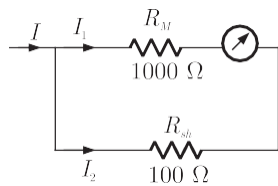
$$\% \text{ Change} = \frac{P_m - P_L}{P_L} \times 100 = \frac{4008 - 4000}{4000} \times 100$$

$$= 0.2\% \text{ more}$$

Sol. 42

Option (C) is correct.

We have to obtain  $n = \frac{I}{I_1}$



$$\frac{I_1}{I_2} = \frac{R_{sh}}{R_m} = \frac{100}{1000} = \frac{1}{10}$$

$$I_1 + I_2 = I$$

$$I_1 + 10I_1 = I$$

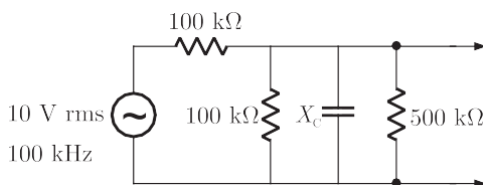
$$11I_1 = I$$

$$n = \frac{I}{I_1} = 11$$

Sol. 43

Option (B) is correct.

In the following configuration



$$\text{Reactance } X_c = \frac{1}{j\omega C} = \frac{1}{2\pi \times 100 \times 10^3 \times 10 \times 10^{-12}}$$

writing node equation at P

$$\frac{V_P - 10}{100} + \frac{V_P}{100} + \frac{V_P}{500} - \frac{j}{159} I = 0$$

$$10 - V_P = V_P(1.2 - j0.628)$$

$$10 = (2.2 - j0.628) V_P$$

$$V_P = \frac{10}{2.28} = 4.38 \text{ V}$$

**Sol. 44** Option (A) is correct.

The torque on the coil is given by

$$\tau = NIBA$$

$$N \text{ " no. of turns, } N = 100$$

$$I \text{ " current, } I = 50 \text{ mA}$$

$$B \text{ " magnetic field, } B = 200 \text{ mT} \quad \text{" Area,}$$

$$A = 10 \text{ mm} \times 20 \text{ mm}$$

$$\begin{aligned} \text{So, } \tau &= 100 \times 50 \times 10^{-3} \times 200 \times 10^{-3} \times 200 \times 10^{-3} \times 10^{-3} \\ &= 200 \times 10^{-6} \text{ Nm} \end{aligned}$$

**Sol. 45** Option (C) is correct.

Meter constant (A-sec/ rev) is given by

$$14.4 = \frac{I}{\text{speed}}$$

$$14.4 = \frac{I}{K \times \text{Power}}$$

Where 'K' is the meter constant in rev / kWh.

$$14.4 = \frac{I}{K \times VI}$$

$$14.4 = \frac{15}{K \times 15 \times 250}$$

$$K = \frac{1}{250 \times 14.4}$$

$$K = \frac{1}{250 \times 14.4} = \frac{1000 \times 3600}{3600} = 1000 \text{ rev / kWh.}$$

**Sol. 46** Option (B) is correct.

For moving iron ammeter full scale torque is given by

$$\tau_c = \frac{1}{2} I^2 \frac{dL}{d\theta}$$

$$240 \times 10^{-6} = \frac{1}{2} (10)^2 \frac{dL}{d\theta}$$

Change in inductance

$$\frac{dL}{d\theta} = 4.8 \text{ mH / radian}$$

**Sol. 47** Option (B) is correct.

In the figure

$$V_{RY} = 415 + 30c$$

$$V_{BN} = \frac{415}{\sqrt{3}} + 120c$$

Current in current coil

$$\begin{aligned} I_c &= \frac{V_{RY}}{Z} = \frac{415 + 30c}{100 + 36.87c} \\ &= 4.15 + -6.87 \end{aligned}$$

$$\sim \text{ power factor} = 0.8$$

$$\cos \phi = 0.8 \quad \& \quad \phi = 36.87^\circ$$

$$\begin{aligned} \text{Power} &= VI \cos \phi = \frac{415}{\sqrt{3}} \times 120 \cos 126.87^\circ \\ &= 994.3 \cos 126.87^\circ = 994.3(-0.60) = -597 \text{ W} \end{aligned}$$

Reading of wattmeter

$$P = 994.3 \cos 126.87^\circ = 994.3(-0.60) = -597 \text{ W}$$

Sol. 48

Option (A) is correct.

For small values of phase angle

$$\frac{I_p}{I_s} = n \sin \phi, \quad \phi \text{ " Phase angle (radians)}$$

$$n \text{ " turns ratio}$$

Magnetizing ampere-turns = 200

$$\text{So primary current } I_p = 200 \times 1 = 200 \text{ amp}$$

$$\text{Turns ratio } n = 500$$

$$\text{Secondary current } I_s = 5 \text{ amp}$$

$$\text{So } \frac{200}{5} = 500 \sin \phi$$

$$\phi \text{ (in degrees)} = \sin^{-1} \left( \frac{200}{5 \times 500} \right) = \sin^{-1} 0.08 = 4.58^\circ$$

Sol. 49

Option (B) is correct.

Voltage appeared at secondary winding

$$E_s = I_s Z_L = 5 \times 1 = 5 \text{ Volts}$$

Voltage induced is given by

$$E_s = \sqrt{2} \pi f N \phi, \quad \phi \text{ " flux}$$

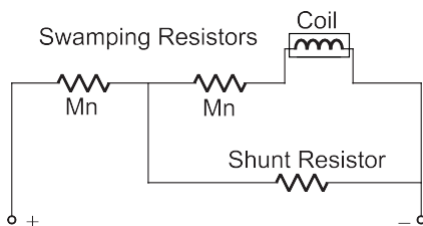
$$5 = \sqrt{2} \times 3.14 \times 50 \times 500 \times \phi$$

$$\phi = \frac{5}{\sqrt{2} \times 3.14 \times 25 \times 10^3} = 45 \times 10^{-6} \text{ wb}$$

Sol. 50

Option (A) is correct.

In PMCC instruments, as temperature increases the coil resistance increases. Swamping resistors are connected in series with the moving coil to provide temperature compensation. Swamping resistors are made of manganin, which has a zero-temperature coefficient.



Sol. 51

Option (C) is correct.

Effect of stray magnetic field is maximum when the operating field and stray fields are parallel.

Sol. 52

Option (A) is correct.

$$\text{Let } C_1 = 300 \text{ pF}$$

$$Q = 120 = \frac{1}{\omega C_1 R}$$

Now when  $C_x$  is connected in parallel with variable resistor  $C_1' = 200 \text{ pF}$

$$Q = 120 = \frac{1}{\omega (C_1' + C_x) R}$$

So  $C_1 = C_1' + C_x$   
 $300 = 200 + C_x$   
 $C_x = 100 \text{ pF}$

Sol. 53

Option (B) is correct.

Maximum frequency of input in dual slope A / D converter is given as

$$T = 2^n T_C$$

$$f_m = \frac{1}{T_m} \text{ " maximum frequency of input}$$

where

$$f_m = \frac{1}{T_C} \text{ " clock frequency}$$

$$c = \frac{f_c}{2^n}, \quad n = 10$$

so

$$f_m =$$

$$\frac{10^6}{1024} = 1 \text{ kHz (approx)}$$

Sol. 54

Option (A) is correct.

Kelvin Double bridge is used for measuring low values of resistances. (P " 2)

Low values of capacitances is precisely measured by schering bridge (Q " 3)

Inductance of a coil with large time constant or high quality factor is measured by hay's bridge ( R " 5)

Sol. 55

Option (C) is correct.

Full scale deflection is produced by a dc current of 1 mA

$$(I_{dc})_{fs} = 1 \text{ mA}$$

For full wave reactifier

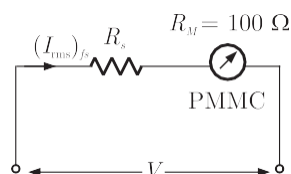
$$(I_{dc})_{fs} = \frac{2I_m}{\pi}, \quad I_m \text{ " peak value of ac current}$$

$$1 \text{ mA} = \frac{2I_m}{3.14}$$

$$I_m = 1.57 \text{ mA}$$

Full scale ac current

$$(I_{rms})_{fs} = \frac{1.57}{\sqrt{2}} = 1.11 \text{ mA}$$



$$V = (R_s + R_m) (I_{rms})_{fs}$$

$$100 = (R_s + 100) (1.11 \text{ mA})$$

$$\frac{100}{(1.11 \text{ mA})} = R_s + 100$$

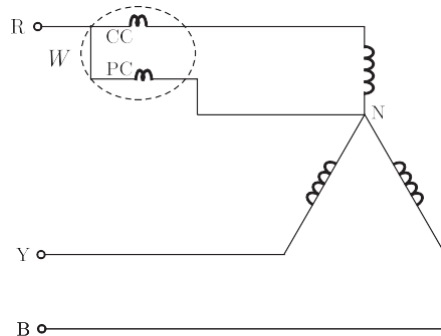
$$100 \neq 900 = R_s + 100$$

$$R_s = 89.9 \text{ kW}$$

Sol. 56

Option (B) is correct.

First the current coil is connected in R-phase and pressure coil is connected between this phase and the neutral as shown below



...(1)

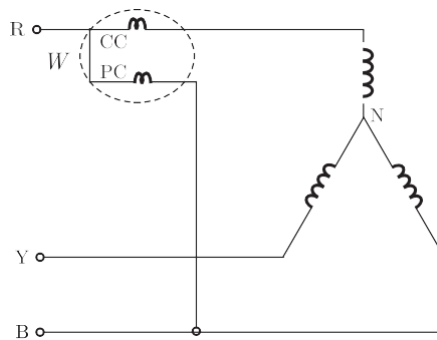
Reading of wattmeter

$$W_1 = I_P V_P \cos \phi_1, \cos \phi_1 = 0.8 \text{ \& } \phi_1 = 36.86^\circ$$

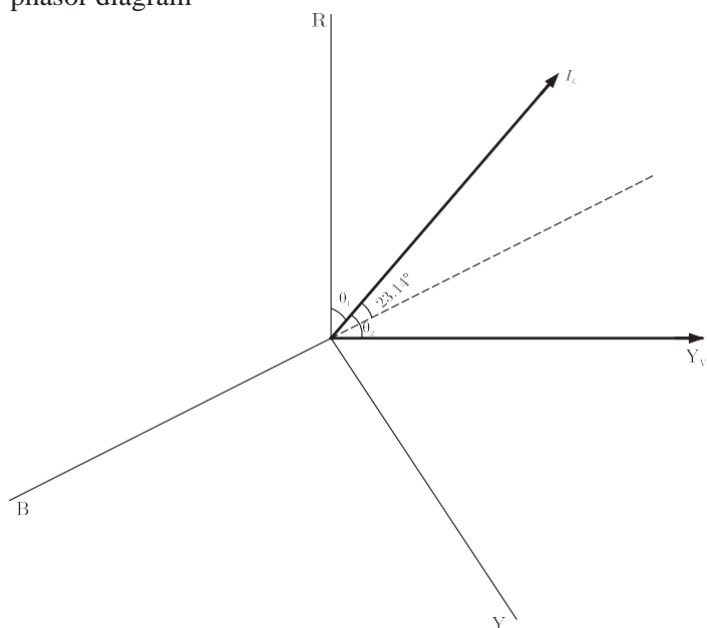
$$400 = I_L \frac{V_L}{3} \cos \phi_1$$

$$400 = \frac{I_L V_L}{3} \times 0.8$$

Now when pressure coil is connected between B and Y-phases, the circuit is



phasor diagram



angle  $\phi_2 = 23.14^\circ + 30^\circ = 53.14^\circ$

now wattmeter reading  $W_2 = V_{YB} I_L \cos \phi_2$

from equation (1)  $V_L I_L = \frac{400 \sqrt{3}}{0.8}$

so  $W_2 = \frac{400}{0.8} \sqrt{3} \cos 53.14^\circ$   
 $= 519.5 \text{ W}$

**Sol. 57**

Option (C) is correct.

In a moving-iron ammeter control torque is given as

$$T_c = K\phi = \frac{1}{2} I^2 \frac{dL}{d\phi}$$

Where

 $K$  = control spring constant $\phi$  = deflection

$$\text{Given that } L = 10 + 3\phi - \frac{\phi^2}{4}$$

$$\frac{dL}{d\phi} = 3 - \frac{\phi}{2} \text{ mH/rad}$$

So,

$$T_c = (25 \times 10^{-6}) \phi = \frac{1}{2} (5)^2 \left(3 - \frac{\phi}{2}\right) \times 10^{-6}$$

$$2\phi = 3 - \frac{\phi}{2}$$

$$\frac{5\phi}{2} = 3 \text{ \& } \phi = \frac{6}{5} = 1.2 \text{ rad.}$$

**Sol. 58**

Option (B) is correct.

$$\text{Magnetizing current } I_m = \frac{250}{1} = 250 \text{ amp}$$

$$\text{Primary current } I_p = 500 \text{ amp}$$

$$\text{Secondary current } I_s = 5 \text{ amp}$$

$$\text{Turn ratio } n = \frac{I_p}{I_s} = \frac{500}{5} = 100$$

$$\text{Total primary current } (I_T) = \sqrt{[\text{primary current } (I_p)]^2 + [\text{magnetising current } (I_m)]^2}$$

$$I_T = \sqrt{I_p^2 + I_m^2}$$

$$= \sqrt{(500)^2 + (250)^2} = 559.01 \text{ amp}$$

$$\text{Turn ratio } n' = \frac{I_T}{I_s} = \frac{559.01}{5} = 111.80$$

$$\text{Percentage ratio error } \mathcal{R}_n = \frac{n - n'}{n'} \times 100$$

$$= \frac{100 - 111.80}{111.80} \times 100 = -10.55\%$$

**Sol. 59**

Option (C) is correct.

Power read by meter  $P_m = VI \sin(\phi - \theta)$ 

Where

$\phi$  Phase angle between supply voltage and pressure coil flux.

$\theta$  Phase angle of load

Here

$$\phi = 85^\circ, \theta = 60^\circ \quad \cos \phi = 0.5$$

So measured power

$$\begin{aligned} P_m &= 220 \times 5 \sin (85^\circ - 60^\circ) \\ &= 1100 \sin 25^\circ \\ &= 464.88 \text{ W} \end{aligned}$$

Actual power

$$P_o = VI \cos \phi = 220 \times 5 \times 0.5 = 550 \text{ W}$$

$$\text{Error in measurement} = P_m - P_o = 464.88 - 550 = -85.12 \text{ W}$$

For unity power factor  $\cos \phi = 1$

$$\phi = 0^\circ$$

So

$$P_m = 220 \times 5 \sin (85^\circ - 0^\circ) = 1095.81 \text{ W}$$

$$P_o = 220 \times 5 \cos 0^\circ = 1100$$

Error in Measurement

$$= 1095.81 - 1100 = -4.19 \text{ W}$$

Sol. 60

Option (A) is correct.

We can obtain the Lissajou pattern (in X-Y mode) by following method.

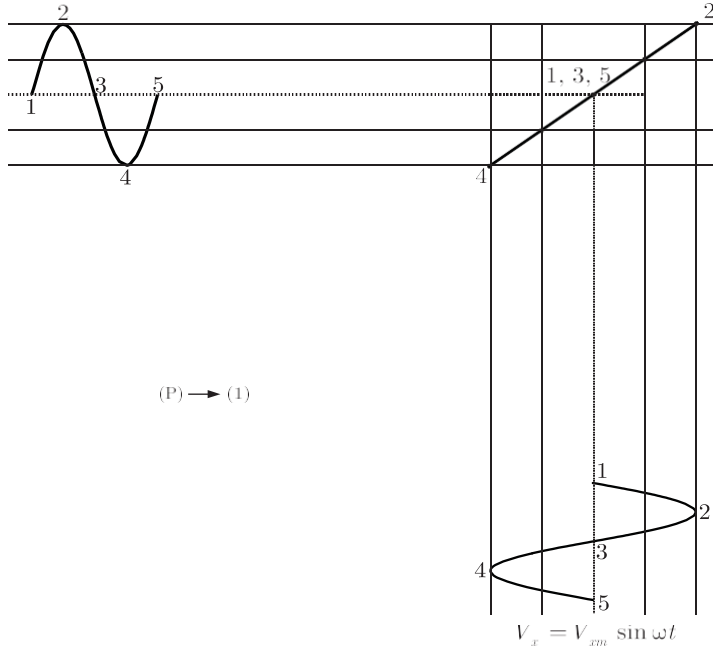
For  $\theta = 0^\circ$ ,

$$V_x = V_{xm} \sin \omega t$$

$$V_y = V_{ym} \sin (\omega t + 0^\circ) = \sin \omega t$$

Draw  $V_x$  and  $V_y$  as shown below

$$V_y = V_{ym} \sin \omega t$$

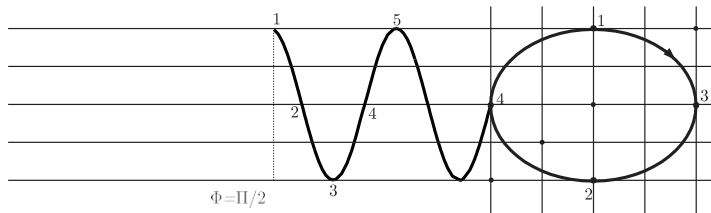


Divide both  $V_y$  and  $V_x$  equal parts and match the corresponding points on the screen.

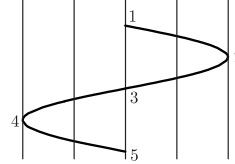
Similarly for  $\theta = 90^\circ$

$$V_x = V_{xm} \sin \omega t$$

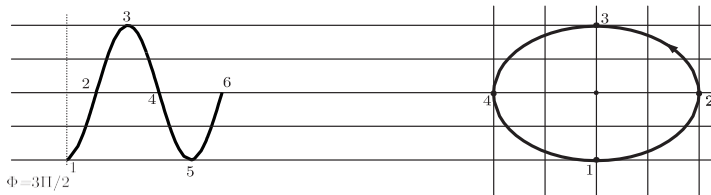
$$V_y = V_{ym} \sin (\omega t + 90^\circ)$$



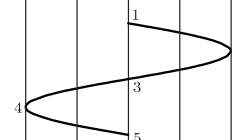
(Q)  $\rightarrow$  (3)



Similarly for  $f = \frac{3p}{2}$



(R)  $\rightarrow$  (6)



we can also obtain for  $0 < f < \frac{3p}{2}$

\*\*\*\*\*